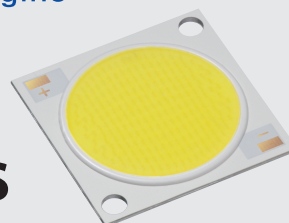


# Heat Dissipation Design

**CITILED**<sup>®</sup>  
The Light Engine



**CLL040 Series**  
\*Including CLL042 Series

Heat dissipation design is a precondition in order to maximize the performance of the LED. In this document, the data that is deemed necessary in the detailed heat dissipation structure of the products and the heat dissipation design of the lighting apparatus is provided as a reference for the appropriate thermal design.

## CONTENTS

1.	Introduction	P.2
2.	Package structure and thermal resistance	P.2
3.	Thermal design outside the package	P.3
4-1.	Simulation ( CLL040-1218A1 )	P.4
4-2.	Simulation ( CLL040-1818A1 )	P.5

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# Heat dissipation structure that can conduct heat radiated from LEDs efficiently

## 1. Introduction

### Significance of the heat dissipation structure

The light-emitting diode of an LED package radiates light and heat according to the input power. However, the surface area of an LED package is quite small, and the package itself is expected to release little heat into the atmosphere. An external radiator such as a heat sink is thus required. The heat dissipation structure up to the connection portion of the external radiator uses mainly heat conduction.

Regarding LED packages, to control the junction temperature of the light-emitting diode  $T_j$  is important. The  $T_j$  must be kept from exceeding the absolute maximum rating in the specifications under any conditions. As direct measurement of the junction temperature of a light-emitting diode

inside a package is difficult, the temperature of a particular part on the external package ( the case temperature )  $T_c$  [ $^{\circ}\text{C}$ ] is normally measured.  $T_j$  [ $^{\circ}\text{C}$ ] is calculated using the thermal resistance between the junction and the case  $R_{j-c}$  [ $^{\circ}\text{C}/\text{W}$ ], and the emitted heat amount that is nearly equal to the input power  $P_d$  [ $\text{W}$ ]. The heat generated at the light-emitting diode can be conducted to the external radiator efficiently because the package structure for the CLL040 series minimizes the thermal resistance  $R_{j-c}$ . This document describes the detailed heat dissipation structure of the CLL040 series and provides data necessary for thermal design of the lighting apparatus to maximize LED performance.

## 2. Package structure and thermal resistance

### Understanding the junction temperature

The cross-sectional structure example, where the package of the CLL040 series is connected to an external heat sink, is shown in Figure-1 ( a ). The package has a laminated structure of an aluminum substrate, insulating layers and conductive copper foil patterns.

A distinctive point is that the light-emitting diode is mounted directly on the well conductive aluminum substrate not on the insulating layer, which has low thermal conductivity. Thus, the heat generated at the light-emitting diode can be efficiently conducted to the outside of the package.

The aluminum substrate side of the package outer shell is thermally connected to the heat sink via heat-dissipation grease ( or adhesive ). As described above, the heat generated in the junction section of the light-emitting diode is transferred mainly to the heat sink using heat conduction, through the light-emitting diode to the adhesive for die-mounting to the aluminum

substrate to the grease ( adhesive ). The thermal resistance between the junction section of the light-emitting diode and the aluminum substrate side of the package outer shell is  $R_{j-c}$ , and the specific thermal resistance value of the package.

Therefore, the following formula is used

$$T_j = R_{j-c} \cdot P_d + T_c$$

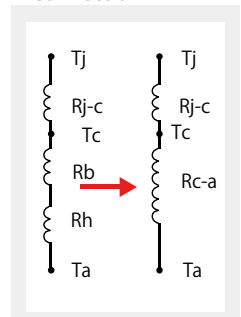
In addition, the thermal resistance of the grease ( adhesive ) outside the package is  $R_b$  [ $^{\circ}\text{C}/\text{W}$ ], the thermal resistance with the heat sink is  $R_h$  [ $^{\circ}\text{C}/\text{W}$ ], and the ambient temperature is  $T_a$  [ $^{\circ}\text{C}$ ].

Figure-2 ( b ) indicates the equivalent thermal resistance along the cross-sectional diagram in Figure-2 ( a ). As indicated, the thermal resistances  $R_{j-c}$ ,  $R_b$ , and  $R_h$  are

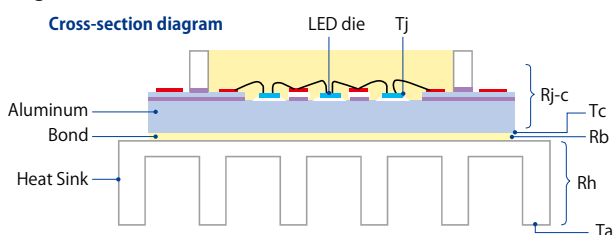
connected in series between the junction temperature  $T_j$  and the ambient temperature  $T_a$ . The thermal resistances outside the package  $R_b$  and  $R_h$  can be integrated into the thermal resistance  $R_{c-a}$  at this point. Thus, the following formula is also used:

$$T_j = ( R_{j-c} + R_{c-a} ) \cdot P_d + T_a$$

**Figure-2 ( a )**  
Thermal Resistance Connection



**Figure-1 ( a ) Cross Section**



# Use the correlation between the thermal resistance and the ambient temperature for design of the external heat dissipation mechanism

## 3. Thermal design of the outside the package

### Point of the external heat dissipation mechanism

The thermal resistance outside the package  $R_{c-a}$  [ $^{\circ}\text{C}/\text{W}$ ], which is the combination of the heat-dissipation grease ( adhesive ) and the heat sink, is limited by the input power  $P_d$  [W], the ambient temperature  $T_a$  [ $^{\circ}\text{C}$ ], and the thermal resistance of the package  $R_{j-c}$  [ $^{\circ}\text{C}/\text{W}$ ], i.e.,

$$T_j = (R_{j-c} + R_{c-a}) \cdot P_d + T_a \rightarrow R_{c-a} = (T_j - T_a) / P_d - R_{j-c}$$

$T_j$  function converted from the above formula is

$$R_{c-a} = -T_a / P_d + T_j / P_d - R_{j-c}$$

and it is a straight line with the slope of  $-1 / P_d$  and the intercept of  $T_j / P_d - R_{j-c}$ .

Figure-2 is the chart showing the relationship between the ambient temperature  $T_a$  and the thermal resistance outside the package  $R_{c-a}$  indicated by driving current, where  $T_j$  is assumed to be  $150^{\circ}\text{C}$  - the absolute maximum rating value in the specifications for the

CLL040-1218A1 package.

The higher the ambient temperature  $T_a$  and the larger the driving current, the smaller the allowable thermal resistance outside the package  $R_{c-a} = R_b + R_h$ .

In brief, the grease ( adhesive ) and the heat sink, with smaller thermal resistance ( this means better heat dissipation ) , are required in order to keep  $T_j$  from exceeding  $150^{\circ}\text{C}$ , the absolute maximum rating in the specifications, if the ambient temperature becomes higher and/or the driving current is larger. Therefore, use Figure-2 as a guide when selecting the external heat dissipation parts, and ultimately conduct thermal verification on actual devices.

The equivalent charts for the CLL040-1818A1 packages are shown in Figure-3 respectively.

Figure-2  $T_a$ - $R_{c-a}$  ( CLL040-1218A1 )

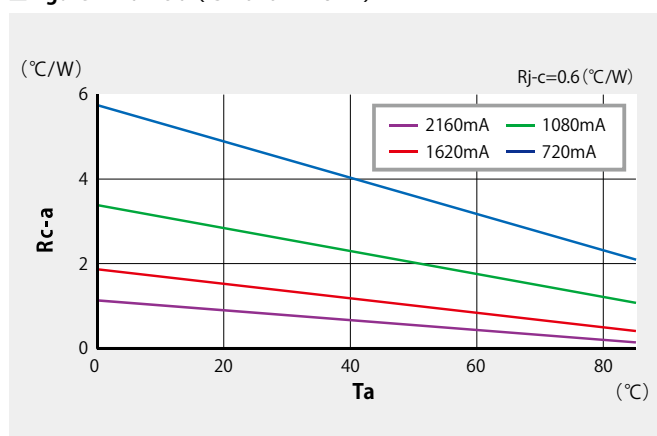
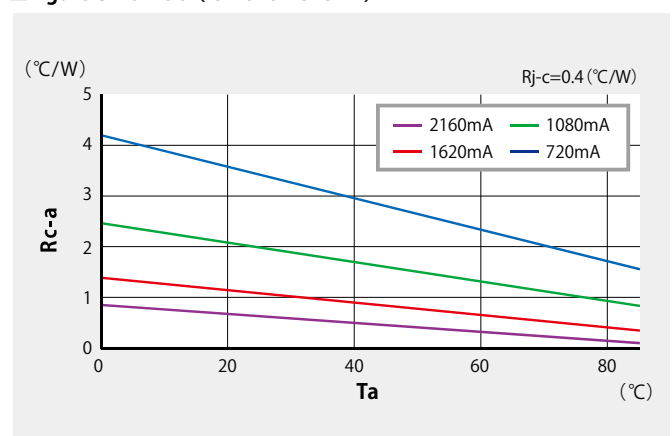


Figure-3  $T_a$ - $R_{c-a}$  ( CLL040-1818A1 )



## 4-1. Simulation ( CLL040-1218A1 )

### For efficient thermal design

A simulation is an effective procedure with regard to the thermal design. Simulation results from when the package of CLL040-1218A1 was connected to the heat sink with a heat conductive sheet are shown in Fig.4 ( a ), ( b ).

#### Boundary conditions

Environmental conditions :  $T_a = 25^\circ\text{C}$

Analysis space :  $400\text{mm} \times 400\text{mm} \times (350+L)\text{mm}$

Wall condition : Top=Open, Others= $25^\circ\text{C}$

Heat dispersion conditions : Natural convection

#### Model conditions

Thermal conductive grease :  $4.5\text{W/m.K}$

Thickness of the heat conductive sheet :  $t=0.12\text{mm}$

Material of the heat sink : Aluminum ( Number of the fin : 6 )

Outline dimensions of the heat sink :  $W\ 64\text{mm} \times H\ 40\text{mm}$

\*Note : sectional area  $1099\text{mm}^2$ , Dimension "L" is variable

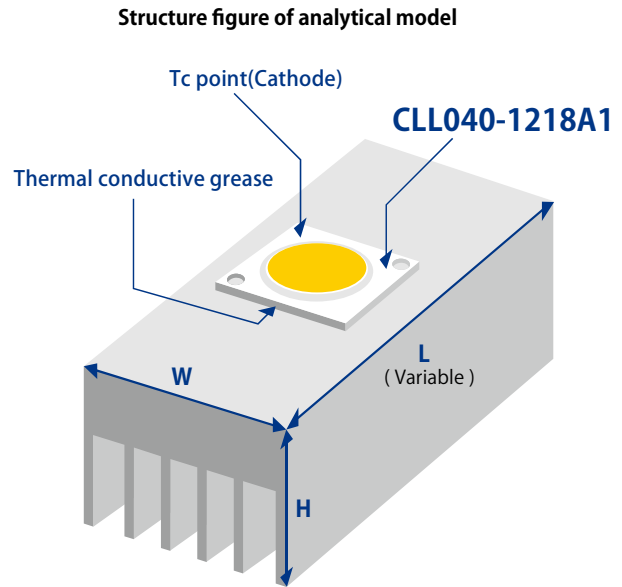


Figure-4 ( a ) Characteristic of heat sink surface area - junction temperature  $T_j$

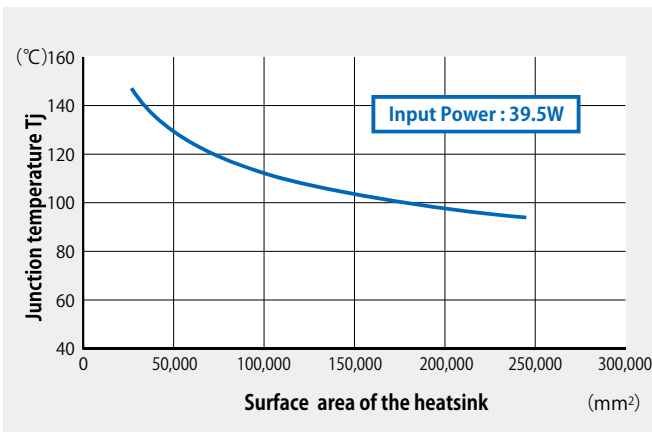
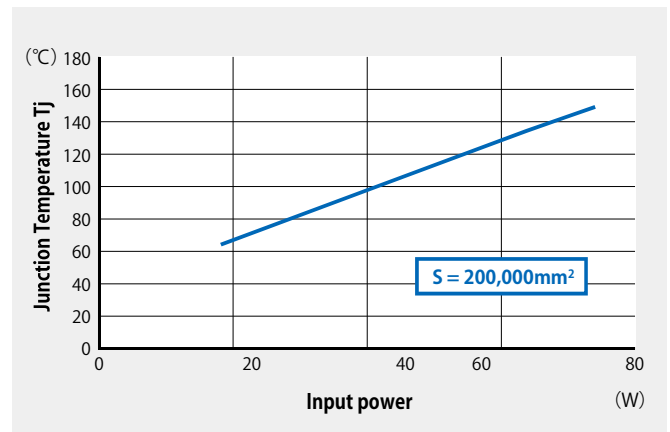


Figure-4 ( b ) Characteristic of input power - junction temperature  $T_j$



\* Above data represents simulation values and is not guaranteed to represent actual measurement values.  
Evaluation and verification shall be conducted under the conditions of actual use.

## 4-2. Simulation ( CLL040-1818A1 )

### For efficient thermal design

A simulation is an effective procedure with regard to the thermal design. Simulation results from when the package of CLL040-1818A1 was connected to the heat sink with a heat conductive sheet are shown in Fig.5 ( a ), ( b ).

#### Boundary conditions

Environmental conditions :  $T_a = 25^\circ\text{C}$   
 Analysis space :  $400\text{mm} \times 400\text{mm} \times (350+L)\text{mm}$   
 Wall condition : Top=Open, Others= $25^\circ\text{C}$   
 Heat dispersion conditions : Natural convection

#### Model conditions

Thermal conductive grease :  $4.5\text{W/m.K}$   
 Thickness of the heat conductive sheet :  $t=0.12\text{mm}$   
 Material of the heat sink : Aluminum ( Number of the fin : 6 )  
 Outline dimensions of the heat sink :  $W\ 64\text{mm} \times H\ 40\text{mm}$   
 \*Note : sectional area  $1099\text{mm}^2$ , Dimension "L" is variable

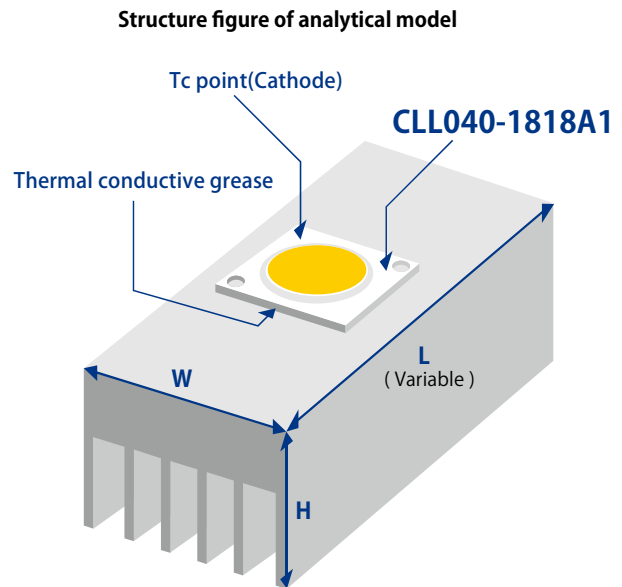


Figure-5 ( a ) Characteristic of heat sink surface area - junction temperature  $T_j$

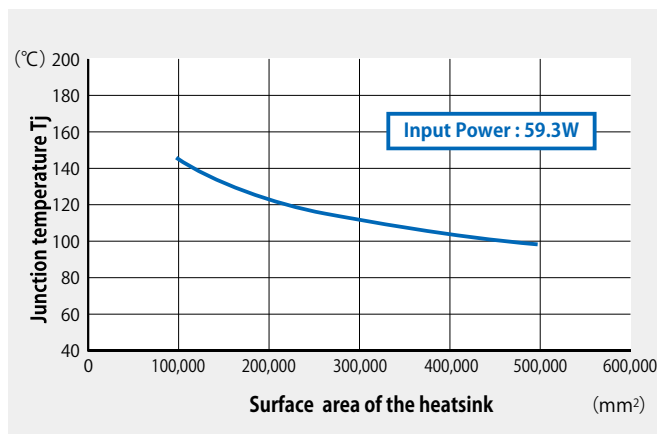
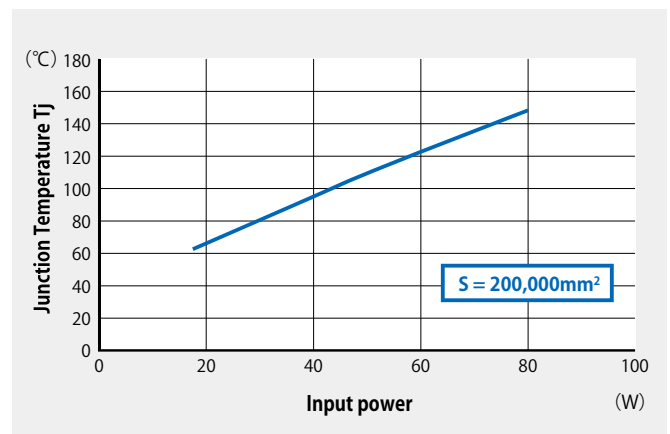


Figure-5 ( b ) Characteristic of input power - junction temperature  $T_j$



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 Evaluation and verification shall be conducted under the conditions of actual use.

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